

Simulation of the capabilities of an orbiter for monitoring the entry of interplanetary matter into the terrestrial atmosphere

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Abstract

In comparison with existing ground-based camera networks for meteors monitoring, a space-based optical system would escape dependency on weather and atmo-

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spheric conditions and would offer a wide spatial coverage and an unrestricted and extinction-free spectral domain. The potential rates of meteor detections by such systems are evaluated in this paper as a function of observations parameters (optical system capabilities, orbital parameters) and considering a reasonable range of meteoroids properties (e.g., mass, velocity, composition) determining their luminosity. A numerical tool called SWARMS (Simulator for Wide Area Recording of Meteors from Space) has been developed. SWARMS is also intended to be used in an operational phase to facilitate the comparison of observations with up-to-date constraints on the flux and characteristics of the interplanetary matter entering our planet's atmosphere. The laws governing the conversion of a fraction of the meteor kinetic energy into radiation during atmospheric entry have been revisited and evaluated based on an analysis of previously published meteor trajectories. Rates of detection were simulated for two different systems: the SPOSH (Smart Panoramic Optical Sensor Head) camera optimized for the observation of transient luminous events, and the JEM-EUSO (Japanese Experiment Module-Extreme Universe Space Observatory) experiment on the ISS (International Space Station). We conclude that up to 6 events per hour in the case of SPOSH, and up to 0.67 events in the case of JEM-EUSO may be detected. The optimal orbit for achieving such rates of detections depends on the mass index of the meteoroid populations. The determination of this parameter appears therefore critical before an optimal orbiting system might be designed for meteors monitoring.

Keywords: Meteors, Photometry

1. Introduction

The most widely used method of observation of meteors is through ground-based camera networks (Halliday et al., 1978; Oberst et al., 1998; Trigo-Rodríguez et al., 2004; Jenniskens et al., 2011; Bland et al., 2012). These observations are complemented by multi-instruments aircraft campaigns for meteor shower events (Vaubailon et al., 2013). A dedicated orbital device would hold considerable advantage over ground-based observations. It would provide wide coverage: for instance, one wide-angle camera with field of view of 120 degrees, at a height of 1200 km would monitor a projected area on the Earth's surface of about 4 millions of km². For example, the 60 cameras of the Meteorite Observation and Recovery Project (hereafter "Canadian Network") were distributed over an area of 1.26 millions of km² (Halliday et al., 1996). Another advantage is the independence from weather conditions. New scientific perspectives would be also offered such as spectroscopy in a wider spectral domain, including UV, which is not possible from the ground due to the atmospheric absorption. Observations using non-dedicated systems, e.g., from military satellites (Brown et al., 2002), have already demonstrated the feasibility and value of orbital observations. Such systems are also envisioned in the context of interplanetary missions (Christou et al., 2012; Mimoun et al., 2012; Oberst et al., 2012; Koschny and McAuliffe, 2009).

We examine here the performance and scientific return of an Earth-orbiting optical system dedicated to the monitoring of meteors. The detection rate is the primary performance parameter of interest and is evaluated as a function of the characteristics of the monitoring device. A simulator, called SWARMS (Simulator for Wide Area Recording of Meteors from Space) has been developed for this pur-

25 pose. The detection rate is determined as a function of observation conditions and
26 of the characteristics of populations of meteoroids defined by mass, composition,
27 and entry velocity distributions. Distributions of meteoroids' physical properties
28 are inferred from previous studies. An empirical law relating physical properties
29 to meteor luminosity is derived from an analysis of a set of 259 meteors for which
30 detailed observations (light curve, meteoroid mass, velocity as a function of time)
31 are available. A script, called SAT (Script for Analysis of meteor Trajectories)
32 was developed for this purpose and will be made available upon request to the
33 corresponding author.

34 The architecture of the software is described in Sec. 2. Section 3 describes SAT
35 and how empirical laws implemented in SWARMS are derived from a set of me-
36 teor observations. Populations of meteoroids are described by their mass index.
37 This parameter is varied in the simulations to study its impact on the system per-
38 formance. The application of SWARMS to two different optical systems, the
39 SPOSH camera and the JEM-EUSO experiment onboard the ISS, are presented
40 in Sec. 4. For the SPOSH camera, the performance of the system is evaluated
41 for different orbits, whereas the ISS orbit is considered for evaluating the per-
42 formance of the JEM-EUSO experiment. The impact of the assumptions on the
43 population of meteoroids (mass index) is also examined. Section 5 is dedicated to
44 conclusions.

45 **2. A Simulator for Wide Area Recording of Meteors from Space (SWARMS)**

46 *2.1. Basic principles of meteor science*

47 All equation parameters with units and definitions are summarized in Table 5.
48 Upon entry into the atmosphere, the kinetic energy E_{kin} of a meteoroid is con-
49 verted into luminous energy according to the following empirical law relating
50 the instantaneous luminous intensity I (in W) and the rate of kinetic energy loss
51 (Nemtchinov et al., 1994):

$$I = -\tau(t, \rho, \dots) \frac{dE_{kin}}{dt}, \quad (1)$$

52 where τ is the instantaneous luminous efficiency. The instantaneous luminous
53 efficiency may vary with meteor properties and with time. It is then convenient
54 to introduce a global luminous efficiency ($\bar{\tau}$), defined as the ratio between total
55 radiated energy and lost kinetic energy (which in most cases is equivalent to the
56 total initial kinetic energy as the meteoroid rarely reaches the ground). Our simu-
57 lations use values of global luminous efficiencies and do not consider the details
58 of the meteoroid trajectories. Optical detectors operate in a finite spectral domain,
59 whereas τ and $\bar{\tau}$ are defined as panchromatic quantities. The spectrum of meteor
60 emissions could vary from one event to another and should affect the estimations
61 of τ or $\bar{\tau}$ from optical observations. As the overwhelming majority of meteor spec-
62 tra available have been limited to the panchromatic visible domain, no definitive
63 conclusion regarding the spectral energy distribution can be drawn. This repre-
64 sents an important source of uncertainty in any simulations using the concept of
65 luminous efficiency.

66 *2.2. SWARMS Specifications*

67 The three major specifications of the simulator are listed below.

- 68 1. A number of assumptions currently made in meteor science may be modi-
69 fied in the future, affecting the calculation of the number and size-distribution
70 of meteoroids, or the estimation of the luminous efficiency from a given
71 meteoroid physical property. New hypotheses or new constraints should be
72 easily implemented.
- 73 2. The detector characteristics must be also tunable in order to facilitate the
74 evaluation of the performance of different optical systems.
- 75 3. The orbital parameters of the mission must be also tunable. It is indeed ex-
76 pected that trade-off between coverage and distance to phenomena (higher
77 orbit increases coverage but meteors will be farther on average and thus
78 appear fainter) should be routinely done for the purpose of optimization.

79 *2.3. Architecture of the simulator*

80 The general architecture of the simulator is shown in Fig. 1. The algorithm is
81 based on the succession of physical processes leading to meteor detection. We
82 used the Python language to develop SWARMS. The step-by-step calculation of
83 a detection rate for a given situation is given in this section.

84 *2.3.1. Step 1: Generation of the survey area*

85 We describe here how the algorithm determines the field of view of the detector,
86 the corresponding area projected on the terrestrial atmosphere, and how this area
87 is meshed.

88 *Generation of mesh:* A mesh representing one hemisphere of the Earth is gen-
 89 erated. Each mesh element has the same surface area. The range of latitudes is
 90 divided into 200 regular intervals. The range of longitudes is also divided into
 91 regular intervals, the number of segments being dependent on the latitude ϕ . The
 92 equator ($\phi = 0$) is divided into $n=1000$ segments. For other latitudes the number
 93 of intervals is equal to $n\cos\phi$ (rounded down). With these parameters, a total num-
 94 ber of $N = 127,924$ mesh elements are generated. The coordinates of each mesh
 95 element are then converted into a cartesian frame with the origin at the center of
 96 the sphere using the average terrestrial radius + 100 km (as meteors usually occur
 97 around this altitude).

98 *Discrimination of points in the field of view:* The field of view of the detector
 99 (Fig. 2) is determined by its orientation (α) with respect to nadir-pointing and
 100 aperture (ω). A mesh including only the N_m elements monitored by the detector
 101 is extracted from the global mesh. The distance between each point P_i at the center
 102 of each mesh element and the detector (O) is then calculated. The surface of the
 103 monitored area is given by:

$$S_{monitored} = \frac{N_m(\alpha, \omega)}{N} S, \quad (2)$$

104 where S is half the surface of the Earth.

105 2.3.2. Step 2: Generation of physical properties of meteoroids

106 A population of meteoroids entering the Earth's atmosphere within the field of
 107 view of the detector and during a given time of observation is generated at this
 108 step. The mass, velocity and density of these meteoroids are randomly assigned
 109 from statistical distributions illustrated in Fig. 3.

110 *Generation of masses:* The mass-distribution is given as a cumulative distribution
 111 function (CDF) providing the number of events above initial mass M_e (initial mass
 112 is the mass of a meteoroid before its entry in the terrestrial atmosphere), per unit
 113 of time and unit of surface. The main CDF used in this study is given in Sec.
 114 3.2.1. The mass index of a population of meteoroids is the value s such as the
 115 number dN of meteoroids with a mass between M and $M + dM$ will be:

$$dN = C_1 M^{-s} dM, \quad (3)$$

116 where C_1 is a constant. The mass index of the distribution we used is thus 1.48
 117 in the low mass branch. Objects are generated on a selected range of masses
 118 (e.g. from 1 μg to 1kg); the lower bound of masses should be chosen based
 119 on the lightest detectable meteoroid in order to avoid unnecessary processing of
 120 numerous undetectable events. The events are generated through the following
 121 steps:

- 122 1. The range of masses (expressed by their logarithm) is divided into inter-
 123 vals of the form $[\log_{10}M_e, \log_{10}(M_e\delta)]$, with $\delta = 1 + \varepsilon$, ε being a value
 124 determined below;
- 125 2. the number of events $N_{events,i}$ on the interval i is determined using the CDF;
- 126 3. for each interval, a uniform distribution in $\log(M_e)$ is generated. The use of
 127 a uniform distribution within the interval introduces an error that depends on
 128 the interval width. By comparing total mass given by the CDF and events
 129 generated in this way, we found that the error remains below 5% at the
 130 condition that $\log(\delta) < 0.25$. The error increases to 10% for $\log(\delta)=0.5$.
 131 A value of $\log(\delta)=0.25$ was selected, resulting in a reasonable duration of
 132 calculation. A higher mass increases the error. The other value examined

133 in this study, 2.17, has been tested and yields an error of 6%. This value of
134 error should be investigated if using a higher mass index, and a reduction in
135 the value of $\log(\delta)$ may be necessary.

136 The number of events in each interval is rounded down. A high-mass interval
137 having a N_{events} value between 0 and 0.5 will therefore not be considered (output
138 of 0 events). This way, the values provided by the simulator are not affected by
139 the possibility of a large event, as the goal is to get typical values to be expected
140 in usual circumstances.

141

142 *Choosing of speed and density:* Velocities V of meteoroids are independently
143 chosen following a Gaussian repartition of $\log V$, reflecting the more frequent oc-
144 currence of slow events, as suggested by radar surveys (Hunt et al., 2004). The
145 mean and standard deviation of the function may be easily changed, and other
146 distribution functions may be implemented in the future. The densities (ρ) of
147 meteoroids are independently attributed following a uniform distribution over a
148 density interval (e.g., from 800 kg/m³ to 4000 kg/m³) that can be modified.

149

150 *Spatial distribution of meteors:* Meteors are considered to appear with a uniform
151 probability over the monitored area. For each event, an elements of the mesh over
152 the field is randomly chosen and the associated distance to the detector is added
153 to the list of the meteor's properties. The list of meteors' properties also includes
154 kinetic energy and size. For instance, for a 100 000 km² surface monitored during
155 100 hours, with a mass distribution from 0.001g to 1kg, the simulator generates
156 63 events, that will or will not be detected (As a function of other hypotheses as

157 per Sec. 4.1).

158 2.3.3. Step 3: Determination of luminous efficiency $\bar{\tau}$

159 In this step, the global luminous efficiency $\bar{\tau}$ is calculated from the assigned me-
160 teoroid properties. The empirical law to calculate $\bar{\tau}$ is determined through the
161 analysis of the Canadian Network meteors (see Sec. 3). The law requires the
162 knowledge of the meteoroid ablation coefficient σ and of its velocity V (Revelle
163 and Ceplecha, 2001). The ablation coefficient σ is calculated from meteoroid
164 density using an empirical inverse-exponential function (see Sec. 3.3).

165 2.3.4. Step 4: Detection

166 The kinetic energy and luminous efficiency, calculated in step 2 and 3, respec-
167 tively, are used to calculate the total luminous energy released by a given event.
168 Then, the minimum detectable luminous intensity I_{min} is deduced from the maxi-
169 mum apparent magnitude detectable by the system and the distance from the event
170 to the system. An event is considered to be detectable if its total energy is suffi-
171 cient to maintain a luminous intensity above I_{min} for the time necessary to appear
172 on a minimum number of frames n_{frames} (set by user). The total energy necessary
173 to fulfill this condition, assuming a steady emission, is given by:

$$E_{min} = I_{min} t_{frame} n_{frames}, \quad (4)$$

174 with t_{frame} being the duration of exposition for one frame. The above calculation
175 assumes that the meteor light emission is steady during the event duration, which
176 is not the case. The shape of the light curve has to be taken into account; it is
177 possible to approximate light curves as a Gaussian function of reduced time. We

178 thus determined a factor F to apply on total luminous energy, so that a gaussian
 179 profile of light curve featuring a total energy of $F \times E_{min}$ would be visible for
 180 as long as a constant emission with a total energy of E_{min} . Thus, equation (4)
 181 becomes:

$$E_{min} = I_{min} t_{frame} n_{frames} F \quad (5)$$

182 The factor F is obtained from a study of a large set of meteors, for which light
 183 curves are available, by calculating the average width of the Gauss curve fitted
 184 to the light curve (see Section 3.3). In order to determine an average shape of
 185 those curves with very different durations, we traced each curve as a function of a
 186 reduced time t_r given by:

$$t_r = \frac{t}{t_{total}}, \quad (6)$$

187 where t_{total} is the total duration of the meteor.

188 3. Analysis of meteors - SAT

189 3.1. Basic differential equations

190 The main equations affecting the evolution of the meteoroid and its trajectory are
 191 the drag equation (7) and ablation equation (8) controlling respectively the change
 192 of mass and velocity (Nemtchinov et al., 1994):

$$M \frac{dV}{dt} = -0.5 \rho_{atmos} V^2 S c_d, \quad (7)$$

193

$$H^* \frac{dM}{dt} = -0.5 \rho_{atmos} V^3 S c_h, \quad (8)$$

194 where M is the mass of the meteoroid, V its speed, ρ_{atmos} is the density of the
 195 atmosphere, H^* is the enthalpy of destruction (required to ablate/erode a unit mass

196 of meteoroid), c_h is a heat transfer coefficient, S is the cross sectional area of the
197 meteoroid, and c_d a drag coefficient. Acceleration due to gravity is neglected in
198 equation (7). Indeed, drag is at least an order of magnitude higher than gravity for
199 a 10cm-sized object of 3500 kg/m^3 density at a typical velocity of 20 km/s. As
200 the object quickly loses altitude, drag rises by several orders of magnitudes with
201 air density (e.g.: 3 orders of magnitude between 120 and 80 km height).

202 On the other hand, variations of height h above ground are given by:

$$\frac{dh}{dt} = -V \sin \gamma, \quad (9)$$

203 where γ is the slope of the trajectory (with respect to the horizon), assuming a
204 linear trajectory during the meteor phase.

205 3.2. Mass distributions from the Canadian Network

206 3.2.1. Photometric and dynamic masses

207 Until more elaborated models were developed (see following section), assessment
208 of mass was done from the luminous intensity (photometric mass) or from the
209 deceleration of the meteoroid (dynamic mass). The two methods are described by
210 [Halliday et al. \(1996\)](#) and applied to the Canadian Network meteors.

211 The photometric mass is determined by considering that a constant fraction of the
212 initial kinetic energy is converted into luminous intensity (using the concept of
213 global luminous efficiency, $\bar{\tau}$). If $\bar{\tau}$ is known, the deduction of the initial kinetic
214 energy is straightforward and, if the initial velocity is known, the initial mass can
215 be easily determined. Values for $\bar{\tau}$ have been determined from masses constrained

216 from meteorite recovery (Halliday et al., 1981) or from infrasonic observations
 217 (Brown et al., 2002). However, $\bar{\tau}$ may vary over several orders of magnitude as a
 218 function of meteoroid properties and the use of a single and constant value for $\bar{\tau}$ is
 219 likely to be incorrect (Revelle and Ceplecha, 2001). Moreover, analysis through
 220 other means (Sec. 3.2.2) indicates that the photometric method may greatly over-
 221 estimate the mass, by as much as three orders of magnitude (Gritsevich and Stulov,
 222 2006).

223 Alternatively, the (dynamic) mass of the meteoroid at a given time may be de-
 224 duced from equation (7) if the velocity V and the deceleration $\frac{dV}{dt}$ are known. This
 225 requires some assumptions on the shape of the meteoroid (governing the values
 226 of S and c_d) and on its bulk density. Assumptions on shape (typically spherical
 227 or brick-like) are not easily justified. Bulk density varies with both composition
 228 and porosity of the body. Another problem is related to fragmentation as dynam-
 229 ical mass assessment applies to the most visible fragment. Moreover, the precise
 230 measurement of instantaneous deceleration is difficult, and some meteors show
 231 little to no deceleration (1/3 of meteors in Halliday et al. (1996)) and thus their
 232 dynamic mass cannot be computed.

233 The mass-distribution of objects entering the Earth's atmosphere has been deter-
 234 mined from photometric masses of the events monitored by the Canadian Network
 235 and can be represented with the two following cumulative distribution functions
 236 (Fig. 3):

$$\begin{cases} \log N = -0.48 \log M_e + 3.3, \text{ with } M_e < 2.4 \text{ kg} \\ \log N = -1.06 \log M_e + 5.26, \text{ with } M_e > 2.4 \text{ kg} \end{cases} \quad (10)$$

237 where N is the number of objects with initial mass above M_e , in grams, per year

238 and million of km² (Halliday et al., 1996).

239 3.2.2. Mass from trajectory analysis

240 More accurate but also more complex methods, taking into account erosion, abla-
241 tion and fragmentation phenomena, offer a better initial mass determination (Ce-
242 plecha and Revelle, 2005). However, this kind of analysis requires precise photo-
243 graphic data and observations of fragmentation events. It explains the discrepan-
244 cies between photometric and dynamic masses by taking fragmentation variation
245 of τ into account. However, as it requires detailed analysis of each meteor (in-
246 cluding light curves and photography) it is not appropriate here. Another method,
247 more easily automated, was recently proposed (Gritsevich, 2009a; Gritsevich and
248 Koschny, 2011). This method is entirely based on the interpretation of variations
249 of speed and height as consequences of braking and mass loss (ablation/erosion).
250 The basic equations of meteor physics (equations 7, 8 and 9) are re-written using
251 the following dimensionless parameters:

$$\left\{ \begin{array}{l} \bar{h} = h/h_0 \\ \bar{V} = V/V_e \\ \bar{M} = M/M_e \\ \bar{S} = S/S_e \end{array} \right. \quad (11)$$

252 where h_0 is the scale height of the atmosphere, M_e the initial mass of the object,
253 V_e the initial velocity, and S_e the initial cross-section. It is assumed that mass and
254 cross section are connected through:

$$\bar{S} = \bar{M}^\mu \quad (12)$$

255 where μ is a coefficient ranging from 0 to 2/3 and representing the effect of the
 256 object's change of shape (related to its rotation, which may distribute heat all
 257 around the surface and prevents shape change) (Gritsevich and Koschny, 2011).
 258 Equation (9) is used in equations (7) and (8) to obtain a system of differential
 259 equations of the velocity and mass as a function of height (time is removed). The
 260 solution of these equations for the non-dimensional mass and height are given by:

$$\bar{M} = \exp\left(-\frac{\beta}{1-\mu}(1-\bar{V}^2)\right) \quad (13)$$

$$\bar{h} = \ln\alpha + \beta - \ln\frac{\Delta}{2}, \quad (14)$$

261 with:

$$\Delta = E_i(\beta) - E_i(\bar{V}^2\beta), \quad (15)$$

262 and

$$E_i(x) = \int_{-\infty}^x \frac{e^z}{z} dz. \quad (16)$$

263 The two dimensionless parameters, α and β represent respectively the efficiency
 264 of atmospheric braking on the meteoroid, and the efficiency of ablation/erosion of
 265 the meteoroid. The expression of these two parameters follow:

$$\alpha = 0.5c_d \frac{\rho_0 h_0 S_e}{M_e \sin\gamma}, \quad (17)$$

266

$$\beta = 0.5(1-\mu) \frac{c_h V_e^2}{c_d H^*}, \quad (18)$$

267 where c_d is the drag coefficient, ρ_0 is the atmospheric density at sea level, S_e is
 268 the initial cross-section area of the object. The values of those two parameters
 269 α and β can be determined empirically by fitting equation (14) to the trajectory
 270 (measured values of \bar{h} and \bar{V}). At this stage, no assumption on meteoroid density
 271 nor shape has to be done. The ablation coefficient σ and initial mass may be then
 272 derived from fitted values of α and β .

273 The ablation coefficient σ is then defined as

$$\sigma = \frac{c_h}{c_d H^*} \quad (19)$$

274 which is the inverse of enthalpy of destruction multiplied by a factor representing
 275 the efficiency with which kinetic energy is converted to heat and transmitted in
 276 the material (ratio c_d/c_h). σ can be deduced from β (equation 18) through:

$$\sigma = \frac{2\beta}{(1-\mu)V_e^2} \quad (20)$$

277 Previous studies also mentioned a link between σ and density ρ as well as with
 278 luminous efficiency τ (Revelle and Ceplecha, 2001). This link is discussed and
 279 used in our analysis of the Canadian Network Meteors in Sec. 3.

280 It is possible to obtain the initial mass M_e through definition of α (see equation
 281 17), with introduction of the shape factor $A_e (= \frac{S_e \rho_m^{2/3}}{M_e^{2/3}})$:

$$M_e = \left(\frac{1}{2} c_d \frac{\rho_0 h_0}{\alpha \sin \gamma \rho_m^{2/3}} \frac{A_e}{\rho_m^{2/3}} \right)^3 \quad (21)$$

282 This requires an assumption on initial shape A_e , drag coefficient c_d and density
 283 (ρ_m) of the meteoroid, but no assumption on other physical parameters such as
 284 heat exchange coefficient or enthalpy of destruction. In this equation:

$$I = \tau \frac{dE_{kin}}{dt} = \tau \frac{dMV^2}{dt}, \quad (22)$$

285 we introduce equation (13) in order to replace M . We then use the definitions of α
 286 from equation (17) and β from equation (18) in order to eliminate M_e . It is then
 287 possible to obtain an equation that links the luminous efficiency τ at a given time
 288 with I (Gritsevich and Koschny, 2011):

$$\frac{\tau(c_d A_e)^3}{\rho_m^2} = \frac{16I\alpha^3 \sin^2 \gamma}{\rho_0^3 V_e^3 h_0^2 f(\bar{V})} \quad (23)$$

289 where $f(\bar{V})$ is a function of the dimensionless velocity:

$$f(\bar{V}) = \bar{V}^3 [E_i(\beta) - E_i(\beta \bar{V}^2)] \left(\frac{\beta \bar{V}^2}{1 - \mu} + 1 \right) \exp\left(\beta \frac{\mu \bar{V}^2 - 1}{1 - \mu}\right) \quad (24)$$

290 Therefore, τ may be determined with equation (23) thanks to measured or empiri-
 291 cally determined parameters (I , \bar{V} , V_e , γ , β , μ), with assumptions on values of
 292 $c_d A_e$ and ρ_m .

293 To summarize, this method can be used to infer the initial mass, luminous effi-
 294 ciency and the ablation coefficient from a least-squares adjustment of the lumi-
 295 nosity and velocity observations to the solution of the equations of atmospheric
 296 entry. Three input parameters need to be known:

- 297 • $c_d A_e$: Unless the shape of the object is known a priori (exceptional case,
 298 e.g., Ayers et al. (1970)) or a meteorite can be retrieved and provide some
 299 hints on the original pre-atmospheric body (Gritsevich, 2008), it can only be
 300 assumed. Example of values found in meteor science are: 1.21 for a body
 301 with an initial spherical shape, 1.55 as in Halliday et al. (1996) or 1.65 used

302 in [Verniani \(1966\)](#) for non perfectly spherical shape, and 1.8 for a brick-like
 303 shape ([Gritsevich and Koschny, 2011](#)), or $c_d A_e = 1.1$ considering a small
 304 c_d for a spherical body ([Wetherill and Revelle, 1981](#); [Revelle and Ceplecha,](#)
 305 [2001](#)).

- 306 • Bulk density of the meteoroid ρ_m : unless a meteorite can be retrieved, it
 307 must be deduced from mechanical properties such as ablation coefficient
 308 σ or be assumed. A typical value of 3500 kg/m^3 , corresponding to the
 309 chondritic density without porosity is often used.
- 310 • μ : By using equations (23) and (24) it is possible to obtain μ by fitting the
 311 measurement of $I(t)$ to:

$$I = \tau \frac{M_e V_e^3 \sin \gamma}{2h_0} v^3 (E_i(\beta) - E_i(\beta v^2)) \left(\frac{\beta v^2}{1 - \mu} + 1 \right) \exp\left(\beta \frac{\mu v^2 - 1}{1 - \mu}\right) \quad (25)$$

312 Further details of the method, justifications and example of applications may be
 313 found in [Gritsevich \(2007\)](#); [Gritsevich and Koschny \(2011\)](#). A very useful exam-
 314 ple of application of this method is proposed in [Gritsevich et al. \(2012\)](#).

315 3.3. Script for Analysis of meteors Trajectories - SAT

316 This script we have created is intended to process a dataset of meteors including
 317 for each time step the time, the height in kilometers above sea level, the veloc-
 318 ity in km/s, the absolute magnitude of the meteor (the distance of reference for
 319 definition of absolute magnitude of a meteor is 100 km), and the estimation of
 320 photometric mass. Deceleration and other values that can be inferred from this

321 set of observation (dynamic mass, density) are added for time steps for which
322 deceleration could be measured. The data is to be entered in csv format.

323 The following parameters are calculated directly from the data by SAT:

- 324 • *Duration* is used to create dimensionless time steps; average duration of
325 meteors is an indication on possible sampling bias (towards longer events
326 due to slow shutter rotation on the cameras of the Canadian Network);
- 327 • *Minimum magnitude* is the minimum absolute magnitude reached by the
328 object,
- 329 • *Constant speed* is a Boolean variable to indicate meteors with no apparent
330 deceleration, in order to assess their number and exclude them from analysis
331 requiring deceleration values;
- 332 • γ is the slope of the trajectory, with respect to the local horizon, calculated
333 step-by-step from velocity, time and height;
- 334 • *PdynInit* is dynamic pressure at the beginning height (first detection) of the
335 meteor. It is calculated from height, velocity, and air density as given by the
336 COSPAR International Reference Atmosphere (CIRA) model (retrieved on
337 British Atmospheric Data Center website in its NetCDF form, more adapted
338 to use with a Python code). This value may be related to mechanical prop-
339 erties of the material;
- 340 • *Accumulated energy at beginning height* is the energy accumulated through
341 air friction from the entry in the atmosphere to ignition and could be related

342 to material properties (Borovička et al., 2007). It is calculated according to:

$$E_s = \frac{1}{2}c_h \frac{V^2}{\sin(\gamma)} \int_{h_{init}}^{\infty} \rho_{atmos}(h)dh \quad (26)$$

- 343 • *Luminous intensity* is deduced from absolute magnitude in panchromatic
344 domain M_{pan} (through $I = 10^{-0.4M_{pan}+3.185}$ (Ceplecha and Revelle, 2005))
345 as a function of time;
- 346 • *Total luminous energy* E_{lum} is obtained through integration of Luminous
347 intensity over time;
- 348 • An *estimation of the luminous efficiency* $\bar{\tau}$ can be calculated using just the
349 total luminous energy with the relation from Brown et al. (2002):

$$\bar{\tau} = 0.1212E_{lum}^{0.115} \quad (27)$$

350 We calculate this value in order to compare the result with values obtained
351 from other methods;

- 352 • The *standard deviation of the Gaussian curve* fitting the light curve of the
353 meteor is obtained through least-squares fitting. This information is needed
354 for statistical assumptions on shape of the light curve of a meteor (see equa-
355 tion 5), and thus to determine the factor F (see Sec. 2.3.4).

356 We have then implemented the method described in Sec. 3.2.2. While α , β and
357 estimation of masses had already been obtained (Gritsevich, 2009b) for the set of
358 Canadian Network meteors analyzed in Sec. 3.4, the implementation into SAT al-
359 lows to perform the calculations with different assumptions (for mass estimation)
360 and combine them with the latest development of the method: the determination

361 of τ as in [Gritsevich and Koschny \(2011\)](#). The determination of mass and lumi-
 362 nous efficiency requires assumption on the density ρ_m . This has been achieved
 363 by inferring ρ_m from ablation coefficient σ . Values determined in [Revelle and](#)
 364 [Ceplecha \(2001\)](#) have been used, coming from analysis of a sample of events for
 365 which precise trajectory measurements were available. As those values are deter-
 366 mined for four groups (and thus represent four couples ρ_m vs σ) we fitted those
 367 values into an empirical inverse-exponential law relating ρ_m to σ :

$$\rho_m = 0.25 + (4.77 \pm 0.17) \exp(-(23.5 \pm 1.4)\sigma) \quad (28)$$

368 The 0.25 value has been arbitrarily fixed to correspond to the apparent asymptotic
 369 value of most fragile meteoroids. This law does not account for the fraction of
 370 low- σ , high- ρ objects represented by the ferrous meteoroids, for which ρ_m could
 371 rise to 8000 kg/m³. The value of σ is required to get ρ_m and must be deduced
 372 from β as seen in Sec. [3.2.2](#), equation (20). β being empirically fitted and V_e
 373 being measured, μ must be calculated. We do so through the least-squares method
 374 (see Sec. [3.2.2](#), equation 25). Through this calculation process, an estimation of
 375 initial mass M_e is obtained. From this point, $\bar{\tau}$ may be determined from the initial
 376 kinetic energy using M_e and V_e and integration of I for the total luminous energy,
 377 or alternatively from an integration over time:

$$\bar{\tau} = \frac{\int_{v_{final}}^1 \tau(v)M(v)V^2 dv}{\int_{v_{final}}^1 M(v)V^2 dv} \quad (29)$$

378 Whereas using equation (29) may detect some problems in velocity measure-
 379 ments¹, it has no special interest and is more complicated, thus we relied on the

¹Erroneous values of velocity could yield negative $\tau(v)$ values, arguing for the rejection of the

380 ratio of the integrated luminous intensity to initial kinetic energy. The output file
381 of data processing is a .csv (comma-separated values) file in which global values
382 (as opposed to values for each time step of a meteor) are given for each meteor.

383 *3.4. The Canadian Network Analysis*

384 *3.4.1. General consideration on the Canadian Network observations*

385 The result of the application of SAT to the Canadian Network meteors is described
386 here with the objective to establish empirical relationships between the luminous
387 efficiency $\bar{\tau}$ and physical properties of meteoroids. The data of the Canadian Net-
388 work were selected as it contains a large number of meteors for which all data
389 required for analysis with SAT are available in [Halliday et al. \(1996\)](#). For in-
390 stance, other data such as the Prairie Network could be used too but need more
391 work to be converted into a usable format from the available pdf. It should be
392 noted that the average duration of Canadian Network meteors is 2.4 s (median
393 value is 1.8 s). This is above the usual average duration of meteors of 0.3 s; due
394 to low shutter rotation speed and sensitivity of cameras, the network is biased to-
395 wards longer, brighter meteors. Also this set of data was oriented towards higher
396 brightness meteors (hence the use of the “fireball” term). About 1/3 of the mete-
397 ors (88 out of 259) do not show any measurable deceleration, as either the body’s
398 inertia was extremely high, or ablation was predominant (drag causing fragmen-
399 tation instead of aerobraking the whole body). The former interpretation would
400 imply very low α values for such events. The critical size of the body to appear
401 as non-decelerating with the accuracy of the Canadian Network may be estimated

entire record

402 from the drag equation (7). Even using the highest density (8000 kg/m³, corre-
403 sponding to a ferrous body) a size of 150km would be necessary. Dominance of
404 the ablation mechanism is therefore the favored explanation to non-decelerating
405 meteors. These non-decelerating bodies are not submitted to SAT (Sec. 3.2.2).
406 It should also be noted that this study is biased towards objects with the highest
407 strength. The generally low value of the ablation coefficient found in Sec. 3.4.2
408 further confirms that. This can explain why it was not possible to distinguish be-
409 tween several groups of meteors based on beginning height or accumulated energy
410 of beginning height, as the majority of meteors of this sample belongs to a single
411 group.

412 3.4.2. Analysis of meteor trajectories

413 SAT allowed us to obtain σ and μ values through the methods described in Sec-
414 tion 3.3. We note that μ values, when it is possible to estimate this parameter,
415 are generally high, with an average value of 0.56 and in 2/3 of the cases a value
416 of 0.65, corresponding to the upper bound permitted when heat is redistributed
417 by rotation to the whole surface of the body (see Fig. 4). This implies that most
418 meteoroids keep their shape during atmospheric entry. Calculation following the
419 methods of Section 3.3 are achieved to assess the mass of meteoroids. As ex-
420 plained previously, determination of mass permits determination of kinetic en-
421 ergy and thus luminous efficiency, which is used in Sec. 3.4.3. Values of mass
422 calculated in this way may differ from photometric evaluations by as much as 3
423 orders of magnitude (Gritsevich and Stulov, 2006). However, a comparison of the
424 masses estimated by the two approaches for the Canadian Network meteors did
425 not reveal any obvious trends, the average value of $\log \frac{M_{phot}}{M_{trajectory}}$ being 0.24, with a

426 standard deviation of 1.2; this does not allow to find a correction to apply to the
 427 distribution. We thus elected to adopt distributions of events from [Halliday et al.](#)
 428 (1996) as a reference for SWARMS, using the cumulative distribution function
 429 given in Sec. 3.2.1. Another important finding is the low ablation coefficient σ
 430 (Fig. 5). While the four groups identified by [Revelle and Ceplecha \(2001\)](#) feature
 431 100σ values spanning a range from 1.4 to 21, most of the values derived here are
 432 clustered below 3. The causes of this repartition are difficult to explain. It can
 433 be due to the "hardest" meteors (ie, with the lowest ablation coefficient) being
 434 the brightest and longest (hence an observation bias from the Canadian Network).
 435 Another possibility would be that high values of sigma would be associated with
 436 low-strength meteors, having high ablation coefficient, and for which deceleration
 437 is too small to be resolved by the Canadian network.

438 3.4.3. Fitting of Luminous efficiency (τ) law to use in simulator

439 Following the conclusions of [Revelle and Ceplecha \(2001\)](#), the luminous effi-
 440 ciency $\bar{\tau}$ is considered to be a function of V_e and ablation coefficient σ . The
 441 parameters A , B , and C of the following empirical law between $\bar{\tau}$ and σ are deter-
 442 mined using least-squares:

$$\bar{\tau} = A(V_e - V_0)^B \sigma^C, \quad (30)$$

443 where V_0 is chosen at 10 km/s, to represent the absence of emission in the panchro-
 444 matic range of a body entering at a low velocity. The following law was obtained:

$$\begin{aligned}
 \ln \bar{\tau} = & -5.278 \pm 0.66 + (0.87 \pm 0.26) \ln(V_e - V_0) \\
 & - (1.46 \pm 0.2) \ln(100\sigma)
 \end{aligned} \quad (31)$$

445 with V_e in km/s. We find that τ is an increasing function of V_e . Values of luminous
446 efficiency inferred from this law are mostly in the 0.1% to 3% range. Those
447 values are lower than calculated in previous works for the group of hardest meteors
448 ($\tau = 5.57\%$)([Revelle and Ceplecha, 2001](#)) As a comparison, the law proposed by
449 [Brown et al. \(2002\)](#) yields values all close to 2%. This law has been fitted to
450 bodies large enough for their kinetic energy to be deduced through infrasonic
451 measurements, and may not be applicable to the smaller ones detected by the
452 Canadian Network.

453 **4. Results and discussion**

454 For the following application that considers the performance of available detec-
455 tors as a function of the orbital parameters, we used both parts of the program
456 described in the previous section. The SAT part, described in [Sec.3](#), allowed us to
457 analyze a sample of meteors to deduce a law linking physical properties to lumi-
458 nous efficiency. It also extracts other quantities that can be used in other analysis.
459 The SWARMS part, described in [Sec. 2.2](#), allows to obtain a number of meteor
460 detection per hour based on the detector used for observation, its positioning, and
461 the assumption on meteoroids (including luminous efficiency law that has been
462 deduced with SAT).

463 *4.0.4. The SPOSH camera*

464 The SPOSH camera ([Fig. 6](#)) has been developed specifically for the purpose
465 of observing transient luminous phenomena from orbit (meteors and noctilucent
466 clouds). Its characteristics are detailed in [Oberst et al. \(2011\)](#), the features that

467 are critical in this study are given in Table 5. Its mass would reach 2.33 kg with a
468 nominal shielding of 3 mm walls (for a 30 krad requirement). The ability to detect
469 an apparent magnitude 6 object moving at $5^\circ/\text{s}$ is a specification of the camera.
470 The actual device has proven to be able to detect meteors as faint as magnitude
471 $m=5.5$ moving at $8^\circ/\text{s}$. For simulations we keep the conservative values of the
472 specifications ($m=6$ at $5^\circ/\text{s}$). We performed simulations for SPOSH with differ-
473 ent altitudes, from 200 km to 5000 km. The lower value allows to be closer to
474 meteors (and thus to detect fainter ones) at the expense of mission duration (at-
475 mospheric drag), coverage, and high angular speed of meteors. Higher altitudes
476 permit wider coverage but reduce the ability to detect fainter meteors. SPOSH is
477 considered at its shortest exposure time (0.06s). Three frames are required for a
478 valid detection.

479 4.0.5. *The JEM-EUSO experiment*

480 The JEM-EUSO experiment ([Ebisuzaki et al., 2011](#)) is dedicated to the detection
481 of high-energy particles colliding with the Earth's atmosphere with a detector in
482 orbit, mounted on the ISS (International Space Station). Its launch date is not yet
483 determined. A case has been made for its use in the detection of other phenomena,
484 including meteors (A. Celino, personal communication). The following remarks
485 can be made about this use:

- 486 1. The mission profile is fixed (orbit at 400 km on the ISS).
- 487 2. The monitoring would be done in the near-UV band: 290 to 430 nm. It is
488 difficult to know what would be the consequence on the rate of detection:
489 meteors may contain a lot of energy in the UV band ([Carbary et al., 2004](#))
490 but the 290 - 430 nm band may be also quite narrow. The difference with

491 the usual panchromatic monitoring of meteors makes difficult to apply cur-
492 rent results to this experience; it is possible that higher energy in this band
493 compensates for its narrowness.

494 3. The field of view of $60^\circ \times 60^\circ$ provides a considerable coverage, albeit less
495 important than SPOSH.

496 4. As its primary mission is the monitoring of high-energy particles, JEM-
497 EUSO has to be able to capture very short events in the μs range. Meteors
498 are "slow" events for this device: angular speed of the object is not a con-
499 cern.

500 5. Reconstruction of trajectory could be possible for the brightest meteors:
501 triangulation could be done on their persistent trains thanks to the orbital
502 motion of the ISS. We have performed a calculation with this configuration
503 and assuming a persistence of the trail of 1s (conservative assumption as
504 trains can last for minutes). Results show that an angular resolution of 0.2°
505 would be required for triangulating the position of a train segment lasting 1s
506 at the maximum distance (determined with optimal tilt for meteor detection
507 as found in Sec. 4.1).

508 6. The JEM-EUSO experiment does not feature a spectrometer, precluding the
509 acquisition of meteor spectra.

510 We have considered the field of view and position (at 400 km) of JEM-EUSO.
511 As there is very few information on the quantity of energy emitted in the near-
512 UV spectrum by meteors, the same requirement on apparent magnitude is held
513 as for visible observations. The requirement on number of frames and duration
514 of exposure (accounted for in the E_{min} calculation) was kept from SPOSH: even
515 though JEM-EUSO has μs exposure time, the time scale of meteor phenomena

516 (deceleration, evolution of light curve) is still around 0.1s.

517 4.1. Simulation results

518 4.1.1. Summary of main assumptions

519 All our simulations are based on the following assumptions.

- 520 • The cumulative distribution function of number of events depending on their
521 mass is taken from the results deduced from Canadian Network observa-
522 tions (Halliday et al., 1996), as seen in Sec. 3.4.2.
- 523 • The distribution of density is uniform between 1000 kg/m³ and 4000 kg/m³.
524 This distribution includes more low density material than suggested by me-
525 teorites recoveries. Meteorite-deduced distributions favor higher values of
526 density due to the toughest materials more often surviving atmospheric en-
527 try. Since low density materials have lower luminous efficiency, our chosen
528 distribution tends to lower the expected number of detections and is a con-
529 servative choice;
- 530 • The distribution of speeds is based on the results of radar surveys, taking
531 into account the bias of detection depending on the speed of entry (Hunt
532 et al., 2004). We elected to use a Gaussian distribution of $\log V_e$, centered
533 on 20 km/s (see Fig. 3).
- 534 • Ablation coefficient σ is deduced from density ρ_m through equation (28).
- 535 • Global Luminous Efficiency $\bar{\tau}$ is deduced from σ and V_e (see Sec. 3.4.3):

$$\bar{\tau} = 0.0051(V_e - V_0)^{0.87} 100\sigma^{-1.46} \quad (32)$$

536 deduced from equation (31).

- 537 • As explained in Sec. 2.3.4, a coefficient F on the minimum energy E_{min} has
538 to be applied to take the shape of light curves into account. Through calcu-
539 lation of the average shape of the light curves of meteors of the Canadian
540 Network, this coefficient has been found to be equal to 18.51. This means
541 that the actual minimum luminous energy of detection is 18.51 times the
542 energy required to detect a theoretical meteor with steady emission during
543 the minimum required time.

544 4.1.2. First use case: the SPOSH camera

545 We have tested a SPOSH camera oriented towards nadir at various altitudes, from
546 200 km (100 km from the atmospheric layer at which meteor occur, conditions
547 similar to observation from ground) to 5000 km. However, due to the presence of
548 radiation belts, a mission above 1800 km is not possible as the satellite would be
549 damaged and eventually put out of order by high-energy particles. Values above
550 this height are only indicated for illustration purposes. The evolution of coverage
551 is shown in Fig. 7. At an height above ground of 1100 km, SPOSH covers the
552 Earth “horizon to horizon”; past this point, increasing the altitude is less effective
553 at increasing coverage, as the Earth does not fill the whole field of view anymore.
554 The detection rates are represented in Fig. 8. The rate of detections rises with
555 orbit height to reach a maximum at 3000 km above ground, with 6 events per hour
556 implying that increased coverage is more important than proximity. The inflection
557 in the curve at 1100km is due to the less favorable evolution of coverage above this
558 altitude. Above 3000 km, distance causes an important loss of apparent magnitude
559 that prevents the detector from seeing the bulk of the meteoroid population.

560 *4.1.3. Second use case: JEM-EUSO experiment*

561 The main difference between SPOSH and JEM-EUSO is the smaller field of view
562 ($60^\circ \times 60^\circ$) of the JEM-EUSO experiment, and the fixed altitude (400 km, altitude
563 of ISS). However, JEM-EUSO may be tilted to increase coverage (but increasing
564 the distance to meteors) so we have simulated different tilt angles, from 0 to 90° .
565 The area covered is roughly $100\,000\text{ km}^2$ when looking towards nadir. Evolution
566 of coverage with tilt angle is given in Fig. 9. The maximum surface area covered
567 is attained a 60° tilt; above that, most of the field of view is above the horizon
568 and thus not suitable for meteor detection. Detection rates are displayed in Fig.
569 10. Due to the relatively low altitude and coverage, the number of detections
570 remains between 0.1 and 0.67 per hour, the latter being for a 60° tilt. As the
571 distance between meteors and the device stays low, the main factor in the number
572 of detection is the surface area covered, as evidenced by the similar shapes of the
573 curves plotted in Fig. 9 and 10.

574 *4.1.4. Effect of mass index of meteoroid distribution*

575 Simulations performed with the distribution deduced from the Canadian Network
576 show that increasing altitude is the best way to maximize the number of detections:
577 wider coverage compensates for increased distance to meteors. However, this
578 conclusion could be altered if a different mass distribution, with a higher mass
579 index, is supposed, as discussed in Sec. 3.2.1. To evaluate how results depend on
580 mass index, we have performed simulations with a mass index of 2.17 deduced
581 from naked-eye meteor counts (Rendtel, 2004):

$$\log N = -1.17 \log M_e + 2.75 \quad (33)$$

582 The 2.75 constant is chosen so that at a height of 200 km, close to conditions of
583 observation from the ground, the number of meteor matched an extrapolation of
584 naked eye counts. However, the main interest of this calculation is to observe the
585 change of trend in number of detections depending on observer's height. Results
586 are illustrated in Fig. 11 and clearly show that under this hypothesis, the lowest
587 orbit possible is optimal regarding the number of detections.

588 It should be observed that the flux we used has been established with a network
589 dedicated to fireballs, so it shouldn't be expected to be accurate at low masses.
590 A distribution established with in-situ detectors of interplanetary dust could be
591 considered instead, such as the one of (Grun et al., 1985). This would imply a
592 mass index of 2.34 (as opposed to 1.48 for Halliday et al. (1996)) at low masses.
593 A combination of the distributions in their respective domains of validity should
594 be considered. Preliminary calculations show that increasing the mass index for
595 bodies below 0.1 g increases the number of detections at low altitude (behavior
596 shown in this section) but that our conclusions are unaffected for an orbit height
597 above 1000km, where the objects below 0.1g are not detected.

598 **5. Conclusions**

599 We have developed SWARMS, a simulator able to predict the number of meteor
600 detections from a space-based dedicated monitoring system. The simulator can
601 take into account different hypotheses on frequency of events, distributions of
602 masses, speeds, and density, on the process leading to light emission. The nu-
603 merical tool may be easily adapted for different observation conditions (including
604 observations around other bodies of the solar system). The meteor parameters

605 used in our simulation derive essentially from the analysis of the meteors detected
606 by the Canadian Network from 1974 to 1985. Our deductions are:

- 607 1. This sample contains mostly hard (low ablation coefficient) meteoroids.
608 Further analysis by considering alternative datasets would be useful to draw
609 more general conclusions.
- 610 2. Estimation of mass through trajectory analysis may differ radically from
611 photometric estimation depending on meteor, but our analysis does not per-
612 mit to reconsider the distribution proposed by [Halliday et al. \(1996\)](#).
- 613 3. We have calibrated a law linking global luminous efficiency to ablation co-
614 efficient and initial velocity. We have found that luminous efficiency is best
615 fitted by an increasing function of velocity. This law gives luminous effi-
616 ciencies mostly in the range of a fraction of a percent to a few percent.

617 Simulations with the chosen distribution of masses show that maximizing cover-
618 age permits a higher rate of detection even if meteor are further and thus fainter.
619 A detector at 1800 km (practical maximum due to radiation belts) should make
620 5.7 detections per hour, against 0.7 detections per hour at 400 km. Low orbits
621 also raise the question of the life expectancy of the mission. Simulations consid-
622 ering the use of JEM-EUSO experiment show that the reduction of field of view
623 affects the rate of detections in a noticeable way (7 times less detections), how-
624 ever, optimal tilting of the detector (towards the limb) increases the number of
625 detections up to 0.67 detections per hour. Those rates of detection would allow to
626 quickly enrich meteor databases; once the mission is operational, SWARMS could
627 be used to fit models on the number and properties of meteoroids (and models of
628 the meteor phenomenon) to observations. However it appears that different distri-
629 butions in meteoroids masses (higher mass index, ie distribution shifted towards

630 higher number of small objects) may reverse the observed trend between the num-
631 ber of detections and the height of the detector. Therefore, a good constraint on
632 the mass index of the target population is critical to decide the optimal height for
633 the mission. This can be achieved thanks to simpler missions dedicated only to
634 meteor counting by nanosatellites (e.g., [Charriet and Fayolle \(2013\)](#)). Next steps
635 to be taken will be to consider the requirements to put on the system for trajectory
636 reconstruction. The practicality and feasibility of reconstructing trajectory from
637 only one point of view (using train persistence and orbital motion of the device)
638 should be studied and could impose new constraints to decide optimal height at
639 which to place the detector. Additionally, the ability to detect the brightest mete-
640 ors during daytime should be investigated. The ideal mission for the monitoring
641 of meteors should include two satellites featuring a wide-angle camera monitoring
642 UV and panchromatic domains in order to maximize the number of detections and
643 permit trajectory reconstruction. It would also include a spectrometer on one of
644 the satellites, as spectroscopy of meteors (especially in UV domain) shows great
645 promise.

646 **Acknowledgements**

647 This research has been funded by CNES through the grant for the project ME-
648 TEOR. The Partenariat Hubert Curien MA/11/257 is also acknowledged for sup-
649 porting the presentation of this work to OISA 2013 at Marrakech. IPPW Student
650 Organizing Committee is acknowledged for supporting presentation of this work
651 at IPPW 10. Maria Gritsevich is supported by the Academy of Finland. Thanks
652 to Daria Kuznetsova and to two anonymous reviewers for useful corrections and
653 comments.

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Table 1: Symbols and parameters used in this paper

Symbol	Unit	Expression/Value	Meaning
α	-	$0.5c_d \frac{\rho_0 h_0 S_e}{M_e \sin \gamma}$	Ballistic coefficient
β	-	$0.5(1-\mu) \frac{c_h V_e^2}{c_d H^*}$	Mass loss coefficient
σ	s^2/m^2	$\frac{2\beta}{(1-\mu)V_e^2}$	Ablation coefficient. Note: 100σ is more often used.
γ	degrees	-	Slope between horizon and trajectory
ρ_0	kg/m^3	-	Atmospheric density at sea level
ρ_{atmos}	kg/m^3	-	Atmospheric density
ρ_m	kg/m^3	-	Meteoroid bulk density.
A_e	-	$\frac{S_e \rho_m^{2/3}}{M_e^{2/3}}$	Meteoroid initial shape factor
A	-	$\frac{S \rho_m^{2/3}}{M^{2/3}}$	Meteoroid shape factor
c_d	-	-	Drag coefficient
c_h	-	-	Heat transfer coefficient
h	km	-	Height of meteoroid
h_0	km	7.16	Scale height of atmosphere
\bar{h}	-	h/h_0	Dimensionless height of meteoroid
H^*	J/kg	-	Effective destruction enthalpy
I	W	-	Luminous intensity of meteor
E_{kin}	J	$0.5MV^2$	Kinetic energy of meteor
$E_{kin,e}$	J	$0.5M_e V_e^2$	Initial kinetic energy of meteor
E_{lum}	J	-	Total luminous energy of meteor
M	kg or g	-	Meteoroid Mass
M_e	kg or g	-	Initial meteoroid Mass
\bar{M}	-	M/M_e	Dimensionless mass of meteoroid
M_{phot}	kg or g	-	Mass of meteoroid evaluated by photometric method
V	km/s	-	Meteoroid velocity
V_e	km/s	-	Initial meteoroid velocity
\bar{V}	-	V/V_e	Dimensionless meteoroid velocity
μ	-	-	Shape change coefficient
τ	-	$I / \frac{dE_{kin}}{dt}$	Luminous efficiency
τ_{global}	-	$\frac{E_{lum}}{E_{kin,e}}$	Global luminous efficiency
S	m^2	-	Cross-section area
S_e	m^2	-	Initial cross-section area

Table 2: Main characteristics of the SPOSH camera, according to [Oberst et al. \(2011\)](#)

Characteristic	Value
Maximum apparent magnitude of detectable object	6
Maximum angular speed of object	$5^\circ/\text{s}$
Field of view	$120^\circ \times 120^\circ$
Minimum exposure time	0.06 s

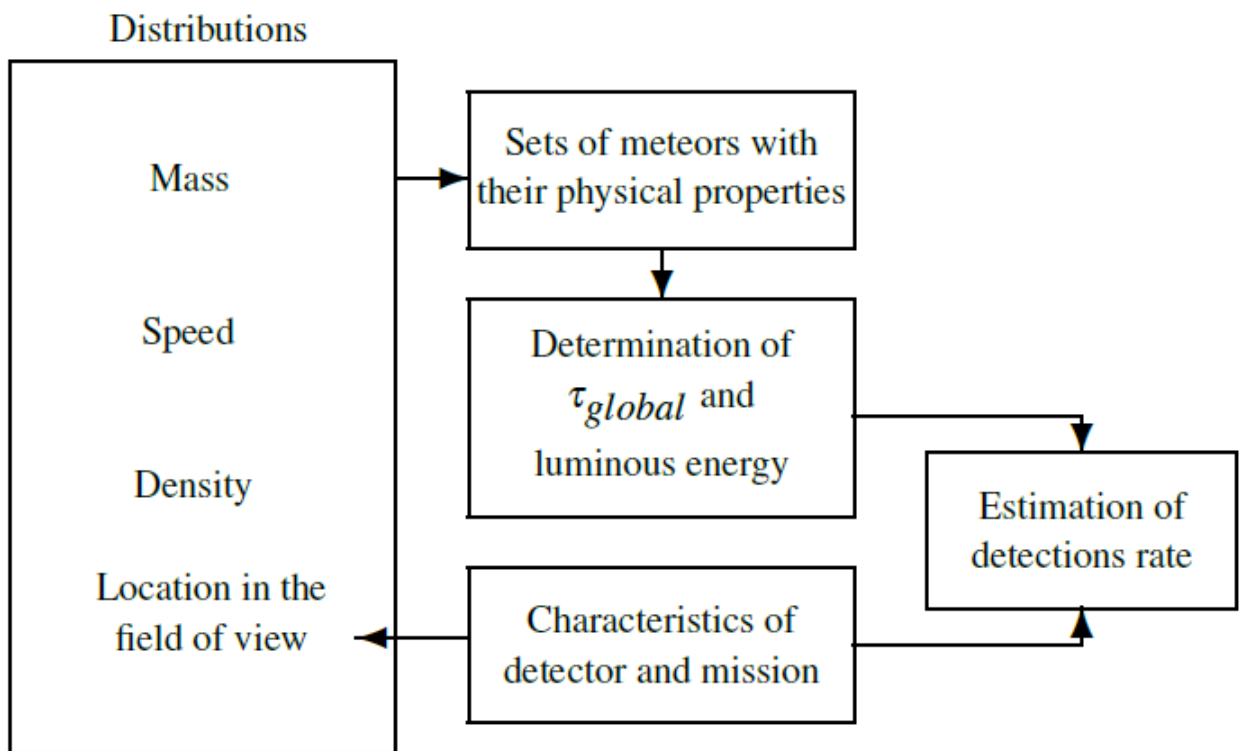


Figure 1: Architecture of the simulator

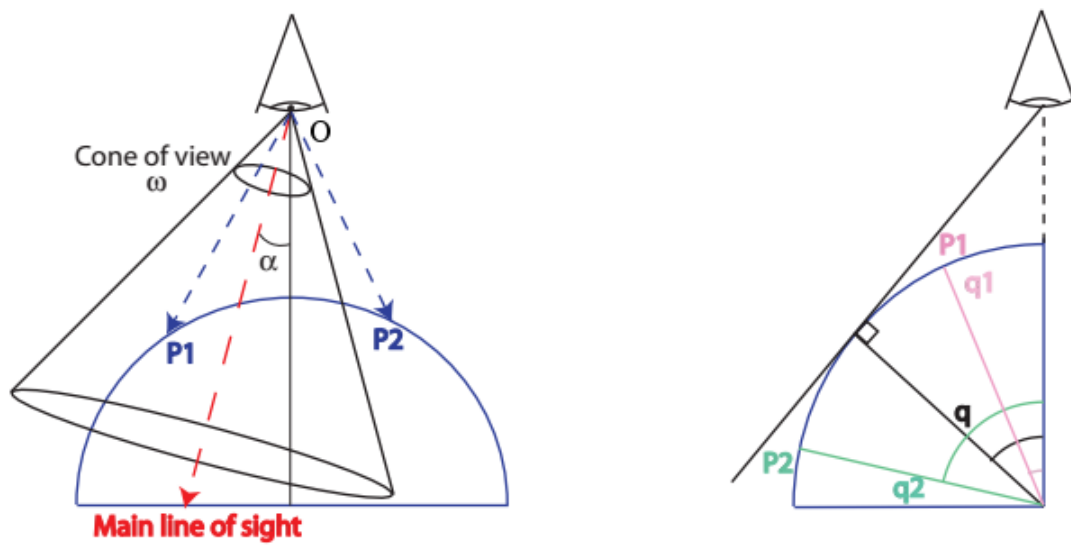


Figure 2: Discrimination of points included in field of view. On the left: For each point P_i , the value of scalar product of \vec{OP}_i with the unitary vector along the main line of sight permits to find the angle between the two and whether P_i is included within the field of view. On the right: The angle θ for a point at horizon depends on detector altitude but is independent of the angle of the line of sight. Once it is calculated, each point P_i verifying $\theta_i > \theta$ is beyond the horizon and must be eliminated.

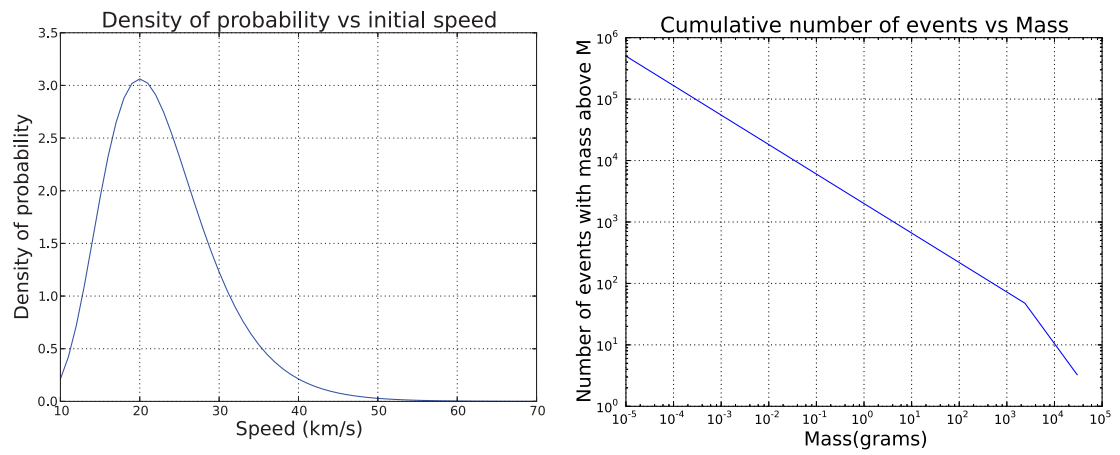


Figure 3: Distributions adopted in initial speeds and initial masses of meteoroids.

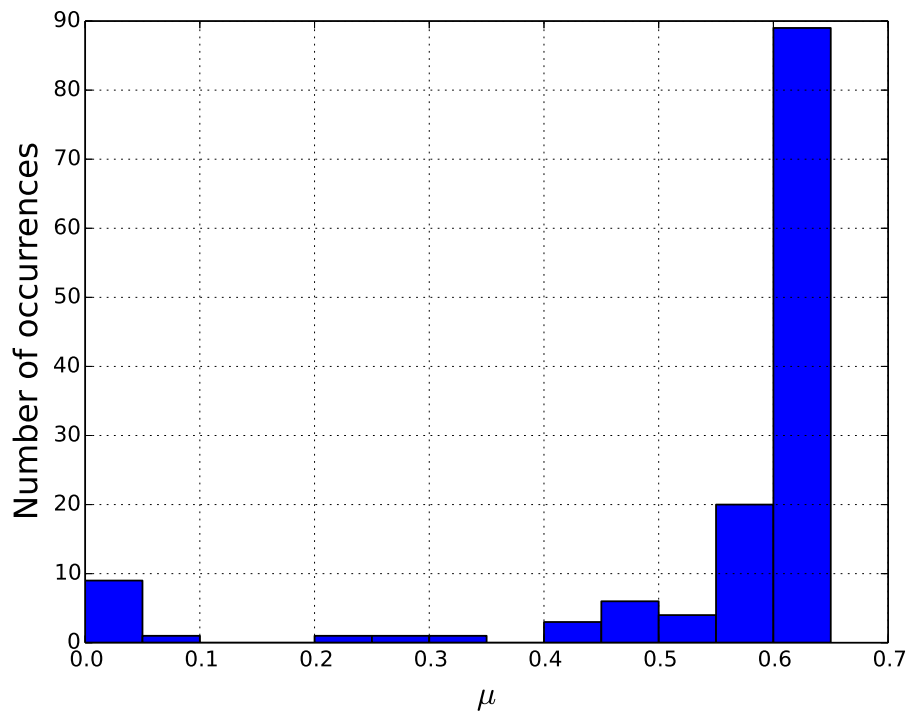


Figure 4: Distribution of values of shape change coefficient μ found through fitting to the light curve in the Canadian Network meteors. 0.65 corresponds to homogeneous distribution of heat by rotation around the meteoroid.

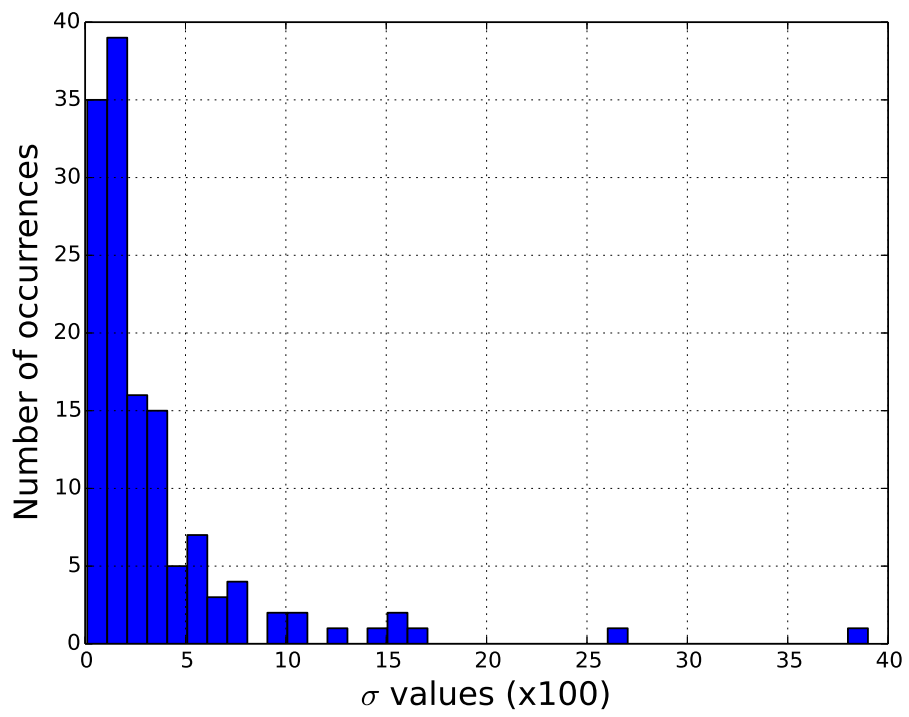


Figure 5: Distribution of values of σ in the Canadian Network meters.



Figure 6: The SPOSH camera

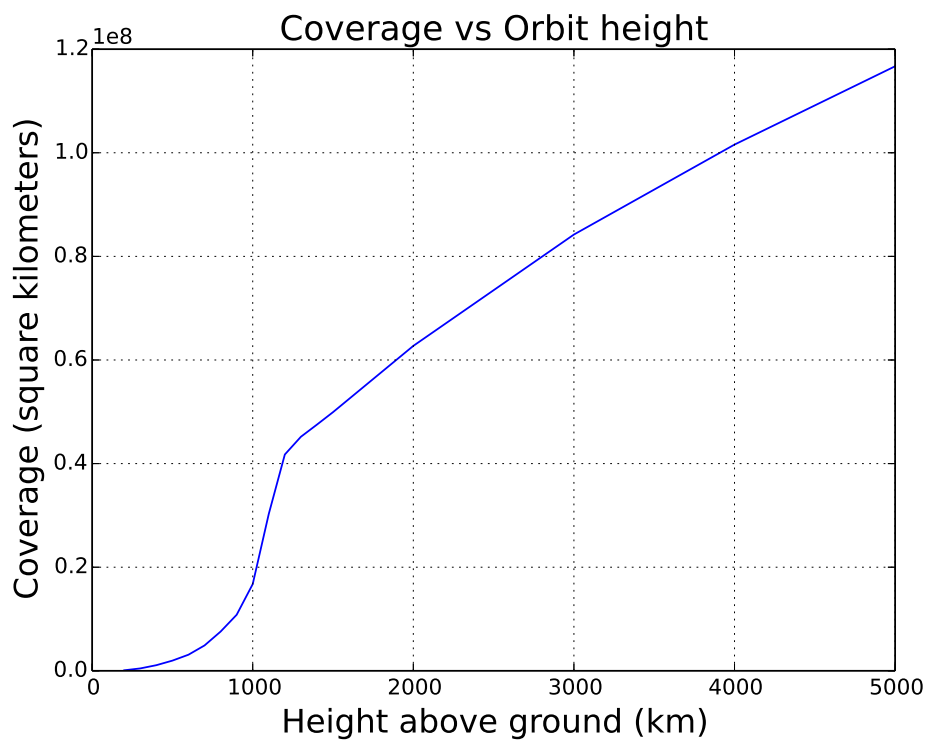


Figure 7: Coverage as a function of orbit height, for a SPOSH camera pointed toward nadir.

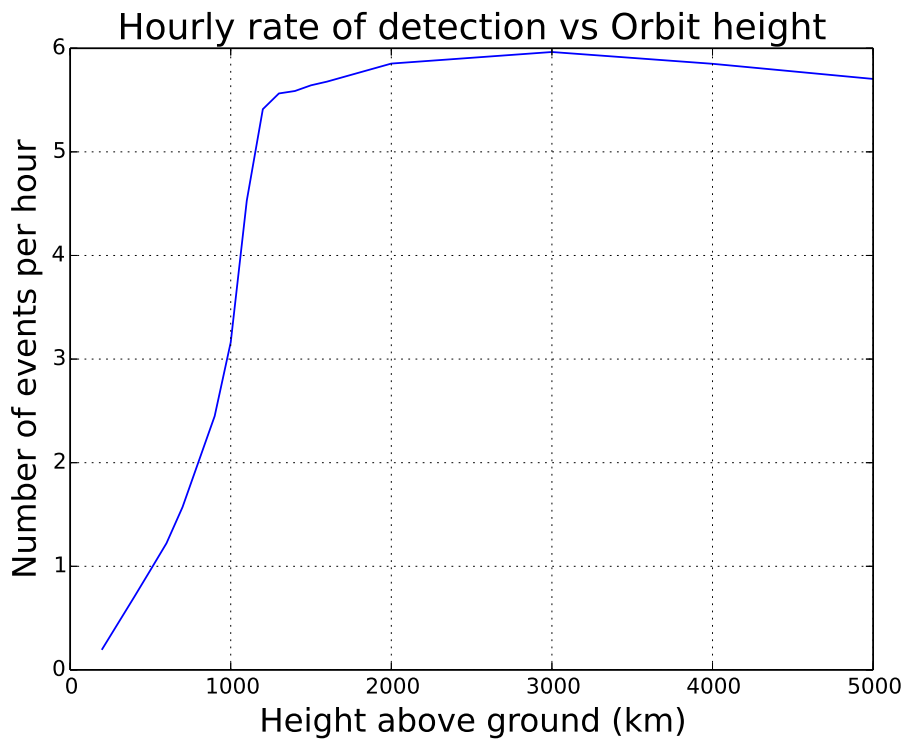


Figure 8: Evolution of hourly rate of detection by a SPOSH camera pointed towards nadir, as a function of orbit height

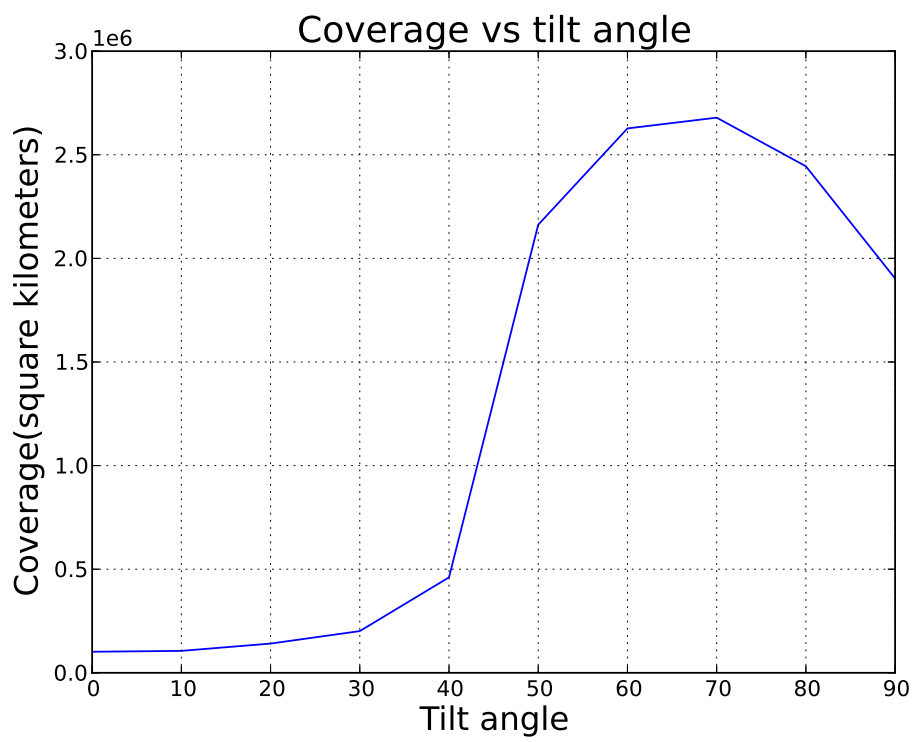


Figure 9: Evolution of coverage by JEM-EUSO as a function of angle of tilt.

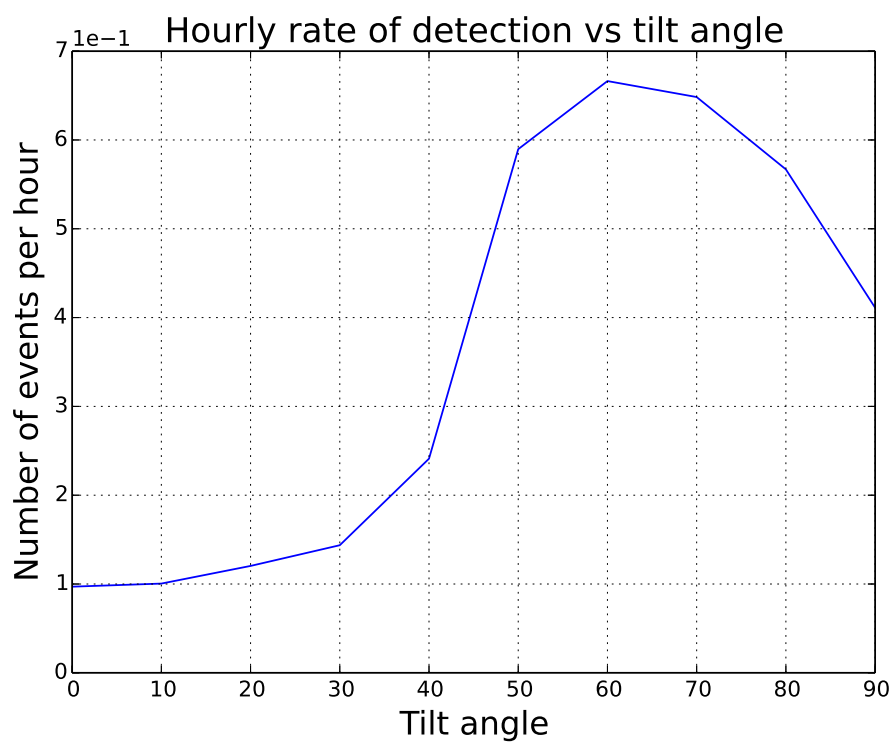


Figure 10: Evolution of hourly rate of detection by JEM-EUSO as a function of angle of tilt.

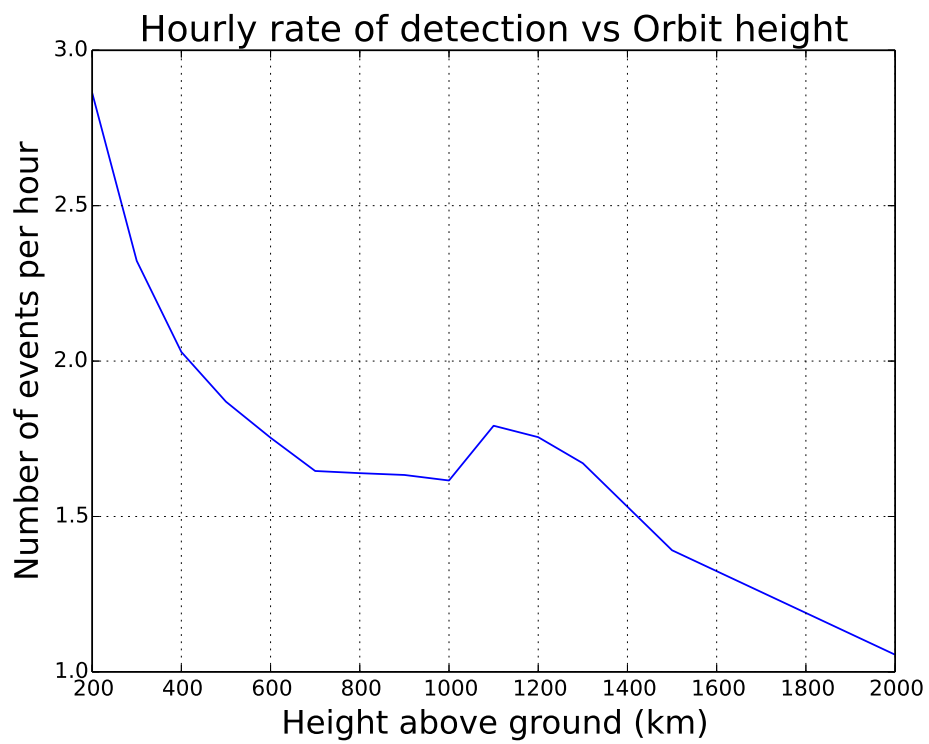


Figure 11: Evolution of hourly rate of detection by a SPOSH camera, assuming a mass index of 2.17, as a function of orbit height